

Journal of Siberian Federal University. Engineering & Technologies, 2017, 10(3), 414-425

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УДК 621.311.245

Reliability Evaluation Method of the Wind-Diesel Installation with Application of Dynamic Fault Tree

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Received 18.05.2016, received in revised form 19.08.2016, accepted 27.12.2016

Renewable energy sources becoming more widespread in decentralized power supply systems. However their functioning depends on the natural resources potential having variable character. This dependence influences reliable work of autonomous power supply system. Reliability analysis of a renewable energy based autonomous generating system is the actual practical task requiring the solution. For the reliability assessment of autonomous wind-diesel installation it is offered to use the method of dynamic fault tree with Markov models for representation of dynamic operators. The offered method is applied for reliability calculation of the wind-diesel installation functioning in the autonomous power supply system in the north of Krasnoyarsk region.

Keywords: renewable energy source, reliability, wind-diesel installation, dynamic fault tree, dynamic operators.

Citation: Tremyasov V.A., Krivenko T.V. Reliability evaluation method of the wind-diesel installation with application of dynamic fault tree, J. Sib. Fed. Univ. Eng. technol., 2017, 10(3), 414-425. DOI: 10.17516/1999-494X-2017-10-3-414-425.

Метод оценки надежности ветродизельной установки с применением динамического дерева отказов

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Возобновляемые источники энергии становятся все более распространенными в децентрализованных системах электроснабжения. Однако их функционирование зависит от потенциала природных ресурсов, имеющих переменный характер. Эта зависимость влияет на надежную работу автономной системы электроснабжения. Анализ надежности автономных систем генерации на основе возобновляемых источников энергии является актуальной практической задачей, требующей своего решения. Для оценки надежности

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автономной ветродизельной установки предлагается метод динамического дерева отказов с использованием марковских моделей для представления динамических операторов. Предложенный метод применен для расчета надежности ветродизельной установки, функционирующей в системе автономного электроснабжения на севере Красноярского края.

Ключевые слова: возобновляемые источники энергии, надежность, ветродизельная установка, динамическое дерево отказов, динамические операторы.

The power sources on the basis of renewable energy sources, such as the sun and wind, gain ground in the world to supply decentralized consumers with electricity. However, the work of renewable energy sources (RES) completely depends on the natural resources potential which possess variable character [1]. Therefore it is necessary to apply RES together with traditional power sources for autonomous power supply of decentralized areas. Usually diesel generators (DG) and storage batteries (SB) are used together with RES. These power sources allow smoothing possible fluctuations of RES power.

Instability of RES electricity production, because of stochastic character of the natural energy resources, influences reliability of autonomous electrical power system. Therefore the reliability analysis of generation systems on the basis of RES is an important and actual practical task requiring solution.

The purpose of this work is the development of the dynamic fault tree method for the reliability analysis of autonomous wind-diesel installation (WDI).

Functioning reliability of the power complex containing RES is defined by reliability indicators of separate elements [2].

The work of wind turbine generator (WTG) is defined by the mode of arriving wind flow and depends on its power characteristics. The main power characteristics of the wind flow are wind speed and annual course of average monthly wind speeds [3].

One of the widespread methods of modeling and reliability prediction of the complex system at the stage of its design is the fault tree (FT) analysis. The FT analysis represents the systematic analysis of events which can cause a system fault, including faults of subsystems and elements, which are the primary causes of system faults [4].

The FT method consists in creation of structural diagram (a fault tree) representing a graphic display of cause-and-effect relationships causing certain types of faults. Event symbols and logical operators are the elements subdividing and connecting a large number of events and conditions, necessary for the fault tree creation. Events and conditions are formulated by specialists according to the system engineering design by means of analysis of its behavior (at emergence of different faults and modes) and the records in the form of conjunctions (\cap) and disjunctions (\cup).

In most cases the purpose of the FT analysis consists in defining probability of a final event. As the final event is the system fault, such analysis gives the probability value of the system fault. The FT structure allows developing algorithms by means of which it is possible to calculate probability of the system fault [5].

For quantitative assessment of the system reliability indicators by means of the FT analysis, the following methods are applied: method of the minimum sections of faults (MSF), methods of mathematical logic, method based on the fault function (FF) [5, 6]. Basic data in the FT method are failure rate λ and repair rate μ of the system elements.

The quantitative FT assessment allows receiving reliability indicators for the system in general. Usually such indicators are: system forced outage rate $q(s)$ and stream parameter of fault $\omega(s)$.

The FT analysis promotes predicting of potential faults and increasing of system reliability on the design stage. Thus, the FT method is a powerful instrument of the reliability analysis of the RES generation system.

In the [7] reliability analysis of autonomous wind-diesel system, the FT method on the basis of MSF allows considering wind turbine fault because of the weather conditions. In this work the classical static fault trees with logical operators AND, OR were used. However the traditional static fault trees cannot capture the behavior of components of complex systems and their interactions such as sequence-dependent of events, spares and dynamic redundancy management, and priorities of failure events.

In order to overcome this difficulty, the concept of dynamic fault tree (DFT) is introduced by adding sequential notion to the traditional fault tree approach. Modeling of dynamic reliability allows overcoming some problems which can arise in the classical fault trees.

DFT is a further development of the traditional FT method by integration of dynamic operators in the fault trees [8]. DFT allows eliminating defects and restrictions of the classical fault trees due to integration of new logical-dynamic operators considering sequence-dependence of events, timing relationships and priorities.

The DFT introduces four basic (dynamic) operators: the priority AND (*PAND*), the sequence enforcing (*SEQ*), the spare (*SPARE*), and the functional dependency (*FDEP*) [1].

The graphic designation and description of the dynamic operators are presented in Table 1.

Integration of dynamic operators in FT allows considering many features of the elements faults in the reliability model leading to emergence of undesirable events, and also technical and organizational measures for reliability ensuring.





Reliability modeling by means of DFT has drawn attention of many engineers working in the field of reliability and safety of complex systems [8].

However, DFT method has some difficulties with respect to the submission of the above dynamic statement.

References [9–13] proposed methods to solve DFT. In reference [9] shown, through a process known as modularization, that it is possible to identify the independent sub-trees with dynamic operators and to use different a Markov model for each of them. However, the solution of a Markov model is much more time and memory consuming than the solution of a standard fault tree model. As the number of components increases in the system, the number of states and transition rates grows exponentially. Development of a state transition diagram can become very cumbersome and a mathematical solution may be infeasible. To reduce state space and minimize the computational time, an improved decomposition scheme where the dynamic sub-tree can be further modularized (if there exist some independent sub-trees in it) is proposed by in [10]. In reference [11] proposed a numerical integration technique for solving dynamic operators. Although this method solves the state-space problem, it cannot be easily applied for repairable systems. In reference [12] proposed a Bayesian network-based method to further reduce the problem of solving DTFs with state-space approach.

In order to overcome limitations of the above-mentioned methods, a Monte-Carlo simulation approach has been attempted in [13] to implement dynamic operators. The Monte-Carlo simulation

Table 1. Dynamic operators

| Designation in DFT | Operator | Description |
|---|----------|---|
|  | $PAND$ | The priority AND (considers sequence of events) |
|  | SEQ | The sequence enforcing (considers sequence-dependence of events) |
|  | $SPARE$ | The spare (considers of the state spare) |
|  | $FDEP$ | The functional dependency (considers sequence of events and timing relationships) |

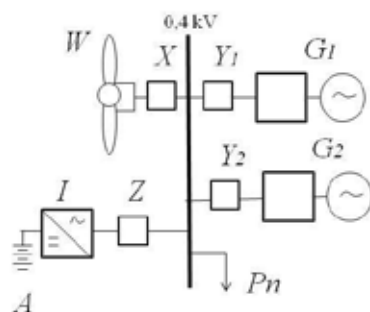


Fig. 1. Autonomous wind-diesel installation: W – wind turbine generator; G_1 – working diesel generator; G_2 – reserve diesel generator; I – inverter; A – storage battery; X, Z, Y_1, Y_2 – circuit breaker; P_n – load

based reliability approach, due to its inherent capability in simulating the actual process and random behavior of the system, can eliminate uncertainty in reliability modeling.

In the autonomous power systems with RES a small number of basic elements is usually used. Therefore for representation of dynamic operators it is possible to apply Markov models.

As an example of the DFT method application for the reliability analysis of autonomous power system, we will consider the scheme of wind-diesel installation (WDI) (Fig. 1), functioning in the northern regions of Krasnoyarsk region taking into account the wind characteristics [3].

WDI includes basic components: the 225 kW wind power unit, the DG system (two diesel generators, 125 kW each) and storage battery with accumulated energy of 100 kW·h.

The wind-diesel complex includes: two diesel generators G_1 and G_2 , the working one and the reserve one. If the working DG G_1 has a fault, then the reserve DG G_2 is automatically started, and the power supply is recovered. It is often supposed that the reserve unit is ready to work every time there is a need of it. For the model to be true to life, we will make an assumption that the reserve unit can sometimes be not ready for work. So, the fault of DG G_2 can happen in attempt of turning it on because of the fault of DG G_1 , and also during inaction of G_2 . Transition of the reserve generator to the

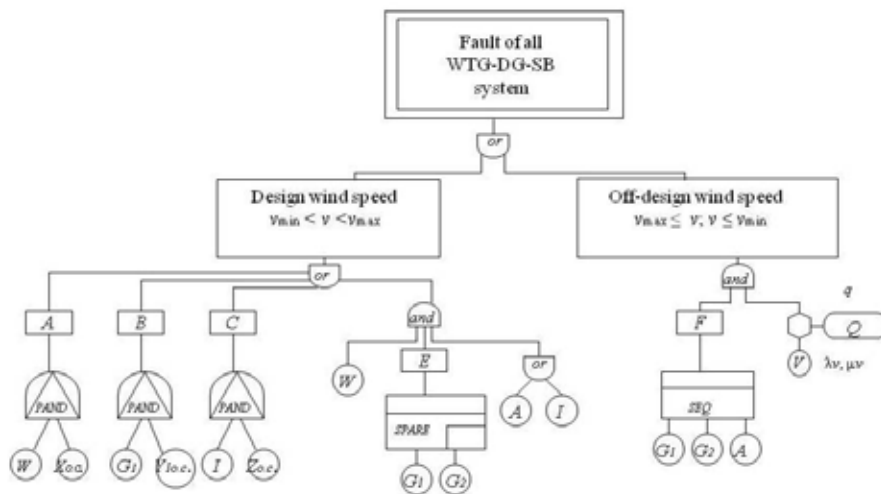


Fig. 2. Dynamic fault tree for reliability analysis of autonomous wind-diesel installation

fault condition will have the fault density equal $\alpha\lambda$, where $\alpha = 0,1$. After repair of DG G_i , it is placed in operation. Reservation of DG increases reliability of the autonomous power system.

Use of storage battery as a part of the power complex is necessary for smoothing of possible fluctuations of WTG power connected with variable character of wind speed.

Let's consider fault events of WDI elements, represented in the Fig. 1. The DFT final event is the "Fault of all WTG-DG-SB system". The corresponding DFT is given in the Fig. 2.

In the reliability analysis of the generation systems, containing WTG, it is necessary to consider wind conditions influencing their functioning. Creation of DFT for WDI considers the design wind speed $v_{\min} < v < v_{\max}$ at which WTG generates power from zero to rated, and the off-design wind speed $v_{\max} \leq v$; $v \leq v_{\min}$ at which WTG does not generate electric power.

When modeling of the design wind speed in DFT the dynamic operators *PAND* and *SPARE* are used. The dynamic operator *PAND* (events at the exit *A*, *B*, *C*) models faults of switches in operation at damage of the corresponding accessions which will lead to the blackout of 0,4 kV collecting bar.

The operator *SPARE* (event at the exit *E*) is applied to modeling of DG system fault. So in case of damage of WTG the working DG can fault, and the attempt to start the reserve DG will not be successful.

Influence of the off-design wind speed on the wind turbine functioning in DFT (Fig. 2) is shown by means of a logical sign "prohibition" (hexagon). Application in DFT of the logical sign "prohibition" allows considering event which happens with some certain probability [5]. In the Fig. 2 the entrance event *V*, placed under the sign "prohibition", is the simple WTG because of wind conditions (lack of wind, a hurricane, etc.). The conditional event *Q*, located sideways from the logical sign, is a restrictive condition which represents a probabilistic weight factor. The restrictive condition is characterized by the value of conditional probability of the off-design wind speed q . The value of the off-design wind speed probability is defined with the help of histogram of wind speed distribution in WDI location. The histogram of wind speed distribution characterizes repeatability of wind speeds for the studied period [3]. It shows how long the wind had a certain speed during the considered period.

Also when modeling of the off-design wind speed in DFT, the dynamic operator SEQ (event at the exit F) is used, which models faults of other system power sources (DG, SB) in the well-defined ordering. There can be no other sequence of faults of these components.

Thus, in DFT of the WTG-DG-SB system three dynamic operators ($PAND$, SEQ , $SPARE$) are used, the representation of which can be executed by means of Markov models [8]. It is necessary to construct a Markov state diagram for each dynamic operator.

Figures 3-5 show the state space diagrams for the DFT dynamic operators described above. Failure and recovery densities are used as the parameters of these models. The shaded states in the diagrams show the system failure. In each state the figures 1 or 0 indicate the work or the fault of the system elements respectively.

On the basis of the constructed diagrams it is possible to make the system of differential equations, the solution of which allows receiving necessary indicators of reliability: probabilities of k conditions of $P_k(t)$ installation and K_G availability factor. In our case from the received system of differential equations for each state space diagram it is necessary to define K_G availability factor for its further use in the DFT analysis.

For calculation of reliability assessment at the initial stage, with rather short time interval, it is necessary to use a non-stationary availability factor. However in most cases it is enough to define a

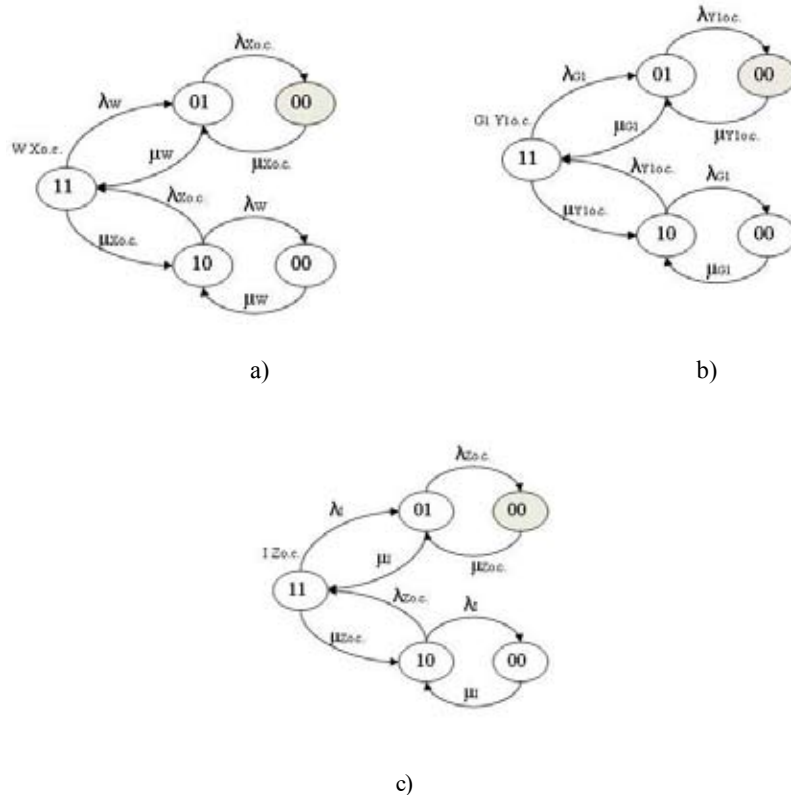


Fig. 3. Markov models for dynamic operators a) $PAND^{(A)}$; b) $PAND^{(B)}$; c) $PAND^{(C)}$: 1 – down state of systems element, 0 – up state; λ – failure rate; μ – repair rate

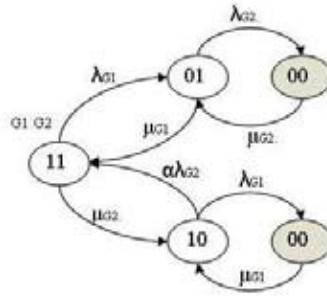


Fig. 4. Markov model for dynamic operator $SPARE^{(E)}$; $\alpha\lambda$ – failure rate for reserve diesel

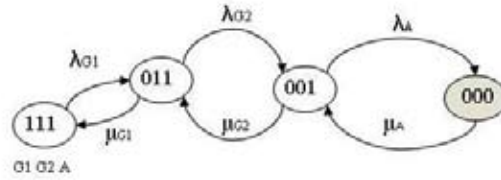


Fig. 5. Markov model for dynamic operator $SEQ^{(F)}$

stationary availability factor – probability that the recovered object will be operable in the randomly chosen timepoint during a steady-state process ($t \rightarrow \infty$).

For each condition k it is possible to write down the following differential equation

$$p'_k(t) = -p_k(t) \sum_{i \in e(k)} \lambda_{ki} + \sum_{i \in E(k)} \lambda_{ik} p_i(t), \quad (1)$$

where $i \in A$ means that summing is conducted under all such states i which belong to a set A ; $E(k)$ – is a set of states from which the direct transition to some state k is possible; $e(k)$ – a set of states to which the direct transition from this state k is possible; $p_i(t)$ – probability of the system stay in i state in t timepoint; λ_{ik} – intensity of transition from the state i to the state k .

If the state graph contains n different states, then n different differential equations can be made as a result. For definition of the availability factor it is necessary to write down n equations and one additional equation of the form

$$\sum_{i=1}^n p_i = 1. \quad (2)$$

According to (1) and (2) we will receive the system of differential equations for definition of the availability factor of the dynamic operator $PAND^{(A)}$

$$\left. \begin{aligned} p'_{11}(t) &= -(\lambda_W + \lambda_{X_{oc}})p_{11}(t) + \mu_W p_{01}(t) + \mu_{X_{oc}} p_{10}(t); \\ p'_{01}(t) &= \lambda_W p_{11}(t) - (\lambda_{X_{oc}} + \mu_W)p_{01}(t) + \mu_{X_{oc}} p_{00}(t); \\ p'_{00}(t) &= \lambda_{X_{oc}} p_{01}(t) + \lambda_W p_{10}(t) - (\mu_{X_{oc}} + \mu_W)p_{00}(t); \\ p_{11}(t) + p_{01}(t) + p_{10}(t) + p_{00}(t) &= 1. \end{aligned} \right\} \quad (3)$$

To solve the differential equations system and to find the required reliability indicator, a computer program in the Mathcad15 environment was used.

As a result of solution of the equations system, we receive values of states probabilities for the dynamic operator $PAND^{(A)}$ and the stationary availability factor using a formula

$$K_G^{PAND(A)} = \sum_{i=1}^3 p_i. \quad (4)$$

Availability factor for this dynamic operator is $K_G^{PAND(A)} = 0,99$.

In the same way let's find the availability factor for other DFT dynamic operators: $K_G^{PAND(B)} = 0,99$; $K_G^{PAND(C)} = 0,99$; $K_G^{SPARE(E)} = 0,99$; $K_G^{SEQ(F)} = 0,98$.

Knowing the availability factor of the dynamic operator K_{Gk}^{DO} , of k , we will define a forced outage rate by the equation

$$q_k^{DO} = 1 - K_{Gk}^{DO}. \quad (5)$$

Thus, the forced outage rate for DFT dynamic operators are respectively equal: $q^{PAND(A)} = 0,01$; $q^{PAND(B)} = 0,01$; $q^{PAND(C)} = 0,01$; $q^{SPARE(E)} = 0,01$; $q^{SEQ(F)} = 0,02$.

The forced outage rate of dynamic operators q_k^{DO} is an indicator of an output event of the corresponding operator and it can be used for the further DFT analysis.

The MSF [5] method is applied for quantitative assessment of DFT given above. This method allows finding such system reliability indicators as the system forced outage rate $q(s)$ and the stream parameter of fault $\omega(s)$.

As the result of DFT analysis, we will receive MSF: A, B, C, WEA, WEI, FV .

As it was stated above, the output event of the dynamic operator (A, B, C, E, F) characterized by the received forced outage rate q_k^{DO} for the corresponding operator.

The forced outage rate for j element of DFT is equal

$$q_j = \frac{\lambda_j}{\lambda_j + \mu_j} [1 - e^{-(\lambda_j + \mu_j)t}], \quad (6)$$

where λ_j – failure rate of j system element, 1/year; μ_j – repair rate of j system element, 1/year.

The stream parameter of fault for j element is determined by a formula

$$\omega_j = \lambda_j (1 - q_j). \quad (7)$$

The probability of existence of i MSF is determined by formulas:
at absence in i MSF of the k dynamic operator

$$q_i^* = \prod_{j=1}^n q_j, \quad (8)$$

at inclusion in i MSF of the k dynamic operator

$$q_i^{*DO} = \prod_{k=1}^m q_k^{DO} \prod_{j=1}^n q_j. \quad (9)$$

The stream parameter of fault for i MSF is determined by formulas:

at absence in i MSF of the k dynamic operator

$$\omega_i^* \approx q_i^* \sum_{j=1}^n \lambda_j / q_j, \quad (10)$$

at inclusion in i MSF of the k dynamic operator

$$\omega_i^{*DO} \approx q_i^{*DO} \sum_{j=1}^n \lambda_j / q_j. \quad (11)$$

Let's determine the stream parameter of fault for the output events A, B, C of the dynamic operator $PAND$ by formulas

$$\begin{aligned} \omega^{PAND(A)} &= \lambda_W (1 - q_W) Q_{X \text{ O.C.}}; \\ \omega^{PAND(B)} &= \lambda_{G1} (1 - q_{G1}) Q_{Y1 \text{ O.C.}}; \\ \omega^{PAND(C)} &= \lambda_I (1 - q_I) Q_{Z \text{ O.C.}}, \end{aligned} \quad (12)$$

where $Q_{o.c.}$ – a conditional probability of switches fault (X, Y, Z) in short circuit clearing in connection, $Q_{X \text{ O.C.}} = Q_{Y1 \text{ O.C.}} = Q_{Z \text{ O.C.}} = 0,5 \cdot 10^{-3} \pm 0,2 \cdot 10^{-3}$.

The stream parameter of fault for the output events E of the dynamic operator $SPARE$ by formulas

$$\omega^{SPARE(E)} = \lambda_{G1} (1 - q_{G1}) Q_{G2 \text{ O.Z.}}, \quad (13)$$

where $Q_{G2 \text{ O.Z.}}$ – a conditional probability of G_2 fault at its start, $Q_{G2 \text{ O.Z.}} = 1 \cdot 10^{-2} \pm 0,5 \cdot 10^{-2}$.

With the off-design wind speed, it is necessary to define the WTG forced outage rate in DFT because of the weather conditions by equation

$$q_V = \frac{\lambda_V}{\lambda_V + \mu_V} \left[1 - e^{-(\lambda_V + \mu_V)t} \right], \quad (14)$$

where $\lambda_V = 1/T_0$ – emergence density of the off-design wind speed, 1/year; $\mu_V = 1/T_N$ – recovery density of the design wind speed, 1/year; T_0 and T_N – the weather periods with off-design and design wind speed respectively [3].

The stream parameter of fault of the WTG connected with wind speed is determined by a formula

$$\omega_V = \lambda_V (1 - q_V). \quad (15)$$

As the entrance event V of the logical sign “prohibition” in FT at the exit gives an event which happens with some certain probability, it is necessary to increase indicators q_v and ω_v by the conditional probability q .

Then the fault probability of WTG because of the weather conditions

$$q_V^* = q_V \cdot q. \quad (16)$$

The expected number of WTG faults in a unit of time

$$\omega_V^* = \omega_V \cdot q. \quad (17)$$

Let's determine the probability of existence of MSF FV with the off-design wind speed by a formula

$$q_{FV}^* = q_V^* q^{SEQ(F)}. \quad (18)$$

Let's determine the failure rate for MSF FV by a formula

$$\omega_{FV}^* = q_V^* \cdot \omega^{SEQ(F)} + q^{SEQ(F)} \omega_V^*, \quad (19)$$

where $\omega^{SEQ(F)}$ – the stream parameter of fault for the output event F of the dynamic operator SEQ which is determined by a formula

$$\omega^{SEQ(F)} = \omega_{G1} q_{G2} q_A + \omega_{G2} q_{G1} q_A + \omega_A q_{G1} q_{G2}. \quad (20)$$

On the basis of the formulas given above, it is possible to determine WDI reliability indicators in general by equations

$$q(s) \approx \sum_{i=1}^{N_s} (q_i^* + q_i^{*DO}) + q_{FV}^*; \quad \omega(s) \approx \sum_{i=1}^{N_s} (\omega_i^* + \omega_i^{*DO}) + \omega_{FV}^*, \quad (21)$$

where N_s – MSF number in WDI with the design wind speed.

The reliability indicators for elements WDI are presented in Table 2 [14, 15]. The necessary meteorological data for accounting of influence of the wind conditions on the work of WDI in DFT and the design values of WTG reliability indicators are provided in the Table 3.

The results of the assessment of WTG reliability for power supply of the northern regions of Krasnoyarsk region are given in the Table 4.

Table 2. Reliability indicators for the WDI elements

| Code elements | Elements WDI | Reliability indicators | | | |
|------------------|--|-----------------------------|-------------------|----------------------|----------------------|
| | | λ_j , 1/year | μ_j , 1/year | q_j | ω_j , 1/year |
| W | Wind turbine generator Vestas V27 225 kW | 1,1 | $3,05 \cdot 10^2$ | $3,61 \cdot 10^{-3}$ | 1,09 |
| G_1 | Working diesel generator | $(2 \pm 0,5) \cdot 10^{-2}$ | $1,0 \cdot 10^2$ | $1,97 \cdot 10^{-4}$ | $1,99 \cdot 10^{-2}$ |
| G_2 | Reserve diesel generator | $(2 \pm 0,5) \cdot 10^{-3}$ | $1,0 \cdot 10^2$ | $1,97 \cdot 10^{-5}$ | $1,99 \cdot 10^{-3}$ |
| I | Inverter | $(5 \pm 4) \cdot 10^{-2}$ | $5 \cdot 10^3$ | $0,99 \cdot 10^{-5}$ | $4,99 \cdot 10^{-2}$ |
| A | Storage battery | $(2 \pm 1) \cdot 10^{-3}$ | $1 \cdot 10^3$ | $1,99 \cdot 10^{-6}$ | $1,99 \cdot 10^{-3}$ |
| X, Y_1, Y_2, Z | Circuit breaker | $(1 \pm 0,5) \cdot 10^{-3}$ | $5 \cdot 10^3$ | $1,99 \cdot 10^{-7}$ | $0,99 \cdot 10^{-3}$ |

Table 3. Meteorological data received for the northern regions of Krasnoyarsk region, and the characteristic of WTG faults

| q | T_o | T_N | λ_V , 1/year | μ_V , 1/year | q_V | q_V^* | ω_V , 1/year | ω_V^* , 1/year |
|------|-------|-------|----------------------|------------------|-------|---------|---------------------|-----------------------|
| 0,05 | 0,42 | 0,58 | 2,38 | 1,72 | 0,57 | 0,0285 | 1,023 | 0,051 |

Table 4. Results of WDI reliability analysis

| MSF | q_i^{*DO} | ω_i^{*DO} , 1/year | $q(s)$ | $\omega(s)$, 1/year |
|------------|------------------------|---------------------------|----------------------|-----------------------|
| <i>A</i> | 0,01 | $5,48 \cdot 10^{-4}$ | $3,06 \cdot 10^{-6}$ | $1,604 \cdot 10^{-3}$ |
| <i>B</i> | 0,01 | $9,98 \cdot 10^{-6}$ | | |
| <i>C</i> | 0,01 | $2,49 \cdot 10^{-5}$ | | |
| <i>WEA</i> | $7,183 \cdot 10^{-11}$ | $9,34 \cdot 10^{-8}$ | | |
| <i>WEI</i> | $3,573 \cdot 10^{-10}$ | $1,91 \cdot 10^{-6}$ | | |
| <i>FV</i> | $5,7 \cdot 10^{-4}$ | $1,02 \cdot 10^{-3}$ | | |

Conclusions

1. The method based on dynamic fault tree for the reliability assessment of wind-diesel installation proposed.
2. The method allows consider failures of a wind-diesel installation caused by weather conditions in its model. Sequence-dependence of events and priorities of failure events can be taken into account due to application of dynamical operators.
3. Reliability of wind-diesel installation is determined by its: forced outage rate $q(s)$ and stream parameter of fault $\omega(s)$, this two indicators can be used to choose optimal structure of WDI.

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